



**PowerTech**  
Belgrade 2023

LEADING INNOVATIONS FOR RESILIENT  
& CARBON-NEUTRAL POWER SYSTEMS

25-29 JUNE, 2023, BELGRADE, SERBIA



UNIVERSIDAD  
POLITÉCNICA  
DE MADRID

POLITÉCNICA

Imperial College  
London

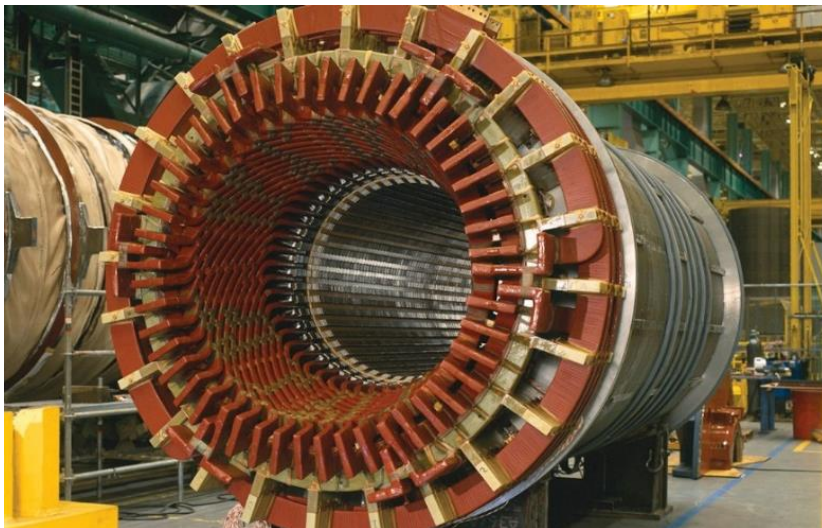
# Assigning Shadow Prices to Synthetic Inertia and Frequency Reserves from RES

*IEEE Trans. on Sustainable Energy, 2023*

Luis Badesa, Carlos Matamala, Yujing Zhou and Goran Strbac

# Lower inertia on the road to lower emissions

Thermal generators  
(nuclear, gas, coal...):



Decarbonisation



Most renewables:  
**no inertia**

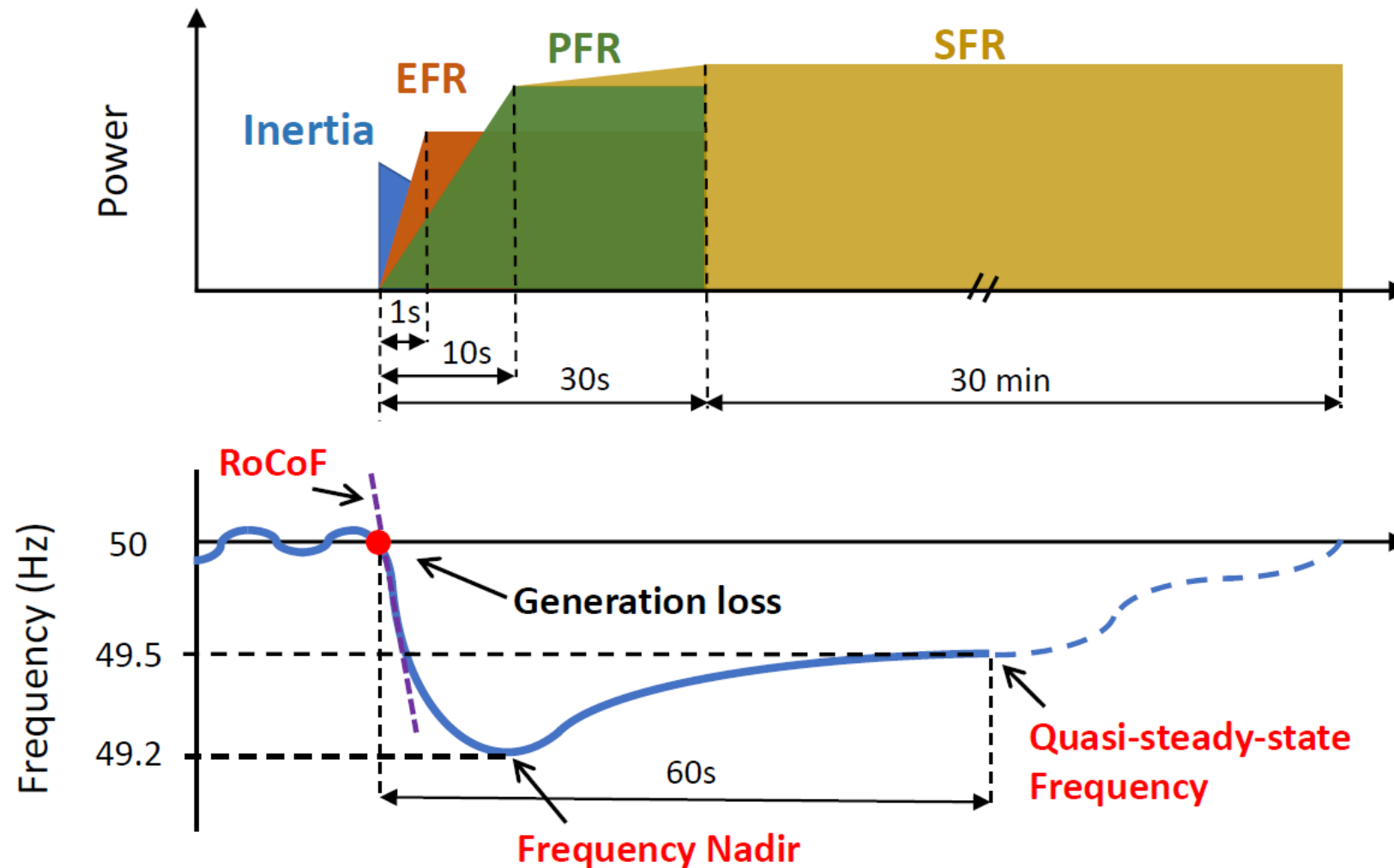


The risk of **instability**  
has increased!

**Inertia stores kinetic energy:**

this energy gave us time to contain a sudden generation-demand imbalance

# How to create incentives for RES to provide ancillary services?



Frequency  
ancillary services  
(**'insurance' to prevent  
blackouts**)

Described by **differential equations**  
(timescale of seconds)

## Swing equation

(reduced-order model for  
system frequency dynamics):

$$\frac{2H}{f_0} \cdot \frac{d\Delta f(t)}{dt} = FR(t) - P_L$$

Economic Optimisation  
(e.g. Unit Commitment)

Based on **algebraic equations**  
(timescale of min/hours)

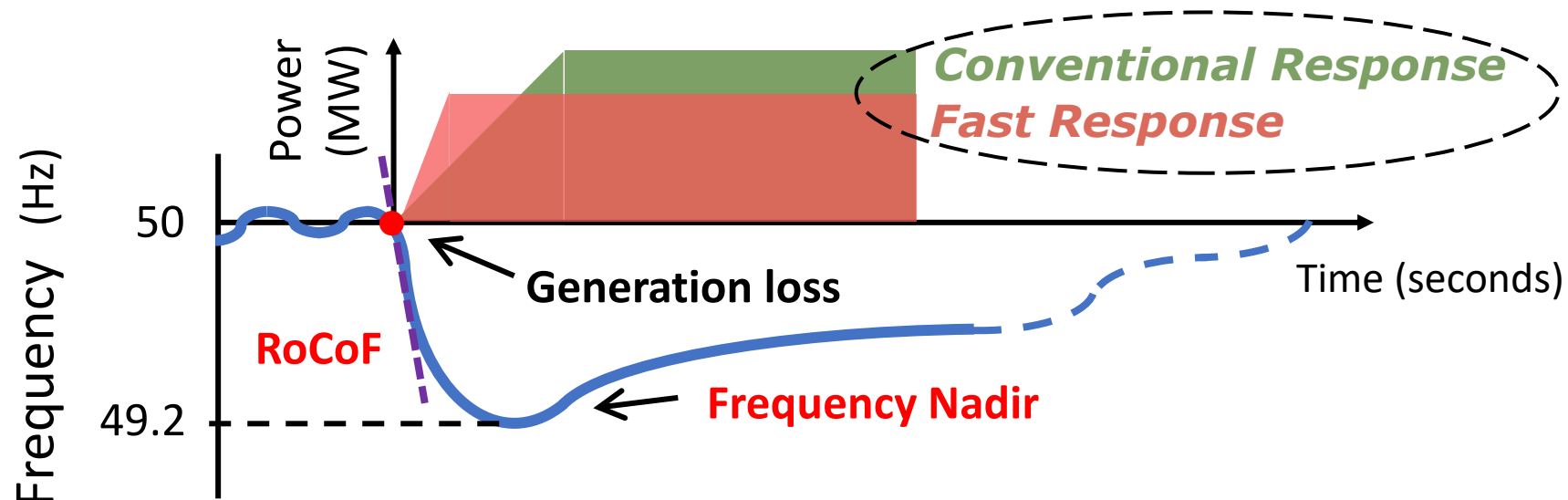
1) Solve swing equation to obtain the  
**conditions for maintaining  
frequency stability**

**2) Compute shadow prices** from  
the dual variables of the  
frequency-security constraints

$$\frac{2(H_{\text{sync}} + H_{\text{synt}})}{f_0} \cdot \frac{d\Delta f(t)}{dt} = \text{FR}(t) - P_L - P_{\text{rec}}(t)$$

Loss of largest power infeed  
(N-1 reliability)

'Recovery effect'  
of wind turbines



$$\frac{2(H_{\text{sync}} + H_{\text{synt}})}{f_0} \cdot \frac{d\Delta f(t)}{dt} = \text{FR}(t) - P_L - P_{\text{rec}}(t)$$

## Simplifications

- Uniform frequency model \*
- Damping is neglected \*\*
- Ramp approximation for frequency response \*\*\*

## Advantages

- Closed form solution
- Convex constraints
- All system magnitudes are decision variables (including ' $P_L$ ')

**Don't like these simplifications?** Then you can refer to these alternative papers:

\* L. Badesa *et al.*, "Conditions for Regional Frequency Stability in Power System Scheduling" (Parts I and II), IEEE Transactions on Power Systems, 2021

\*\* L. Badesa *et al.*, "Simultaneous Scheduling of Multiple Frequency Services in Stochastic Unit Commitment", IEEE Transactions on Power Systems, 2019

\*\*\* M. Patuere *et al.*, "Stochastic Unit Commitment in Low-Inertia Grids", IEEE Transactions on Power Systems, 2020

The simplifications are **only needed when formulating the market**

Additional **advantage** → **Simple and clear instructions** to market participants:

- Comply with a certain ramp requirement for frequency reserves
- Comply with the promised inertia constant

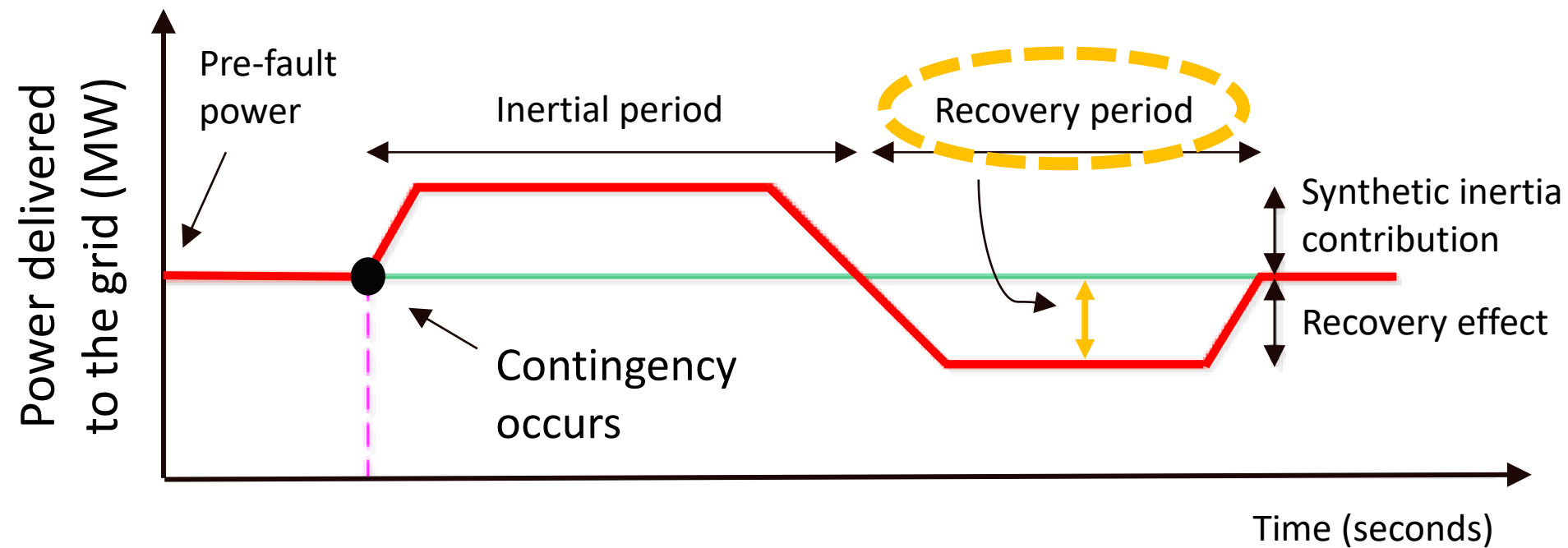
---

A **full dynamic model** would however be used **for tuning the controllers** of the different devices



The **wind turbine decelerates**, so it **deviates from the MPPT**:

- The **power delivered** to the grid by the turbine in the 'post-inertial' period is **lower than the power in the 'pre-fault' period**





## Modelling tool: Frequency-secured Unit Commitment

$$\min \sum_{g \in \mathcal{G}} c_g^{\text{nl}} \cdot y_g + c_g^{\text{m}} \cdot P_g \longrightarrow \text{Minimise fuel and commitment costs}$$

$$\text{s.t.} \quad \sum_{g \in \mathcal{G}} P_g + \sum_{\forall i} (P_i - P_i^{\text{curt}}) = P_D \longrightarrow \text{Load-balance constraint}$$

$$y_g \in \{0, 1\}$$

$$y_g \cdot P_g^{\text{msg}} \leq P_g \leq y_g \cdot P_g^{\text{max}}$$

$$0 \leq R_g \leq y_g \cdot R_g^{\text{max}}$$

$$0 \leq R_g \leq P_g^{\text{max}} - P_g$$

$$0 \leq P_i^{\text{curt}} \leq P_i$$

$$0 \leq R_i \leq R_i^{\text{max}}$$

$$0 \leq R_i \leq P_i^{\text{curt}}$$

Sync. inertia from all  $g$

Synt. inertia from all GFM

RoCoF constraint

Nadir constraint

q-s-s constraint

**Technical characteristics of generators**

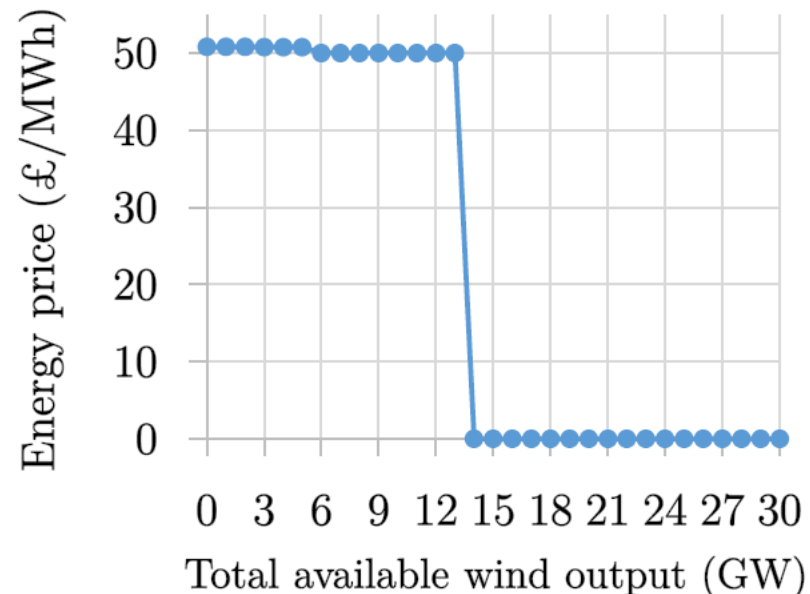
**Ancillary services from generators**

**Frequency-security constraints**

Synthetic inertia from wind turbines with grid-forming inverters has the **same price signal as synchronous inertia**, except when the '*recovery effect*' of the wind turbine is too high

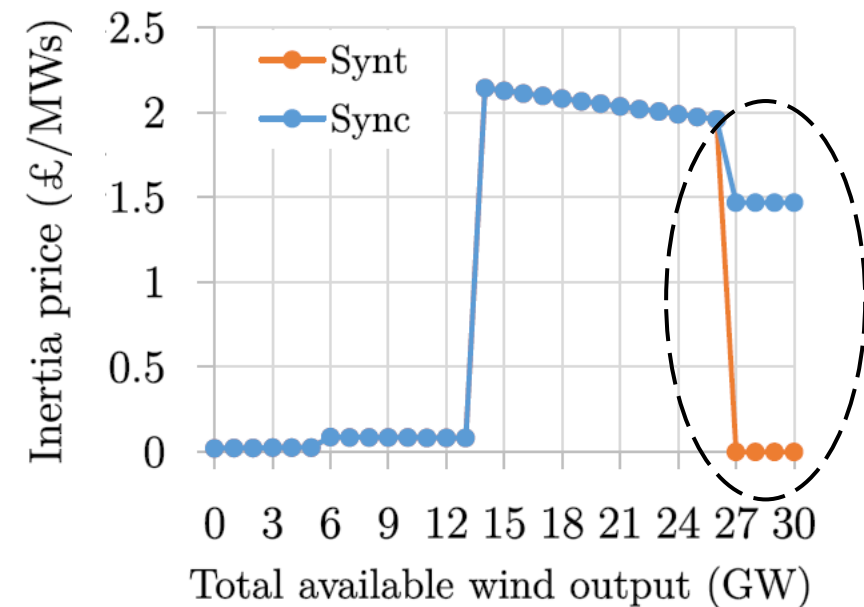
Price for synchronous inertia:

$$\frac{\mu - \lambda_1}{f_0} + 2\lambda_{\text{RoCoF}}$$



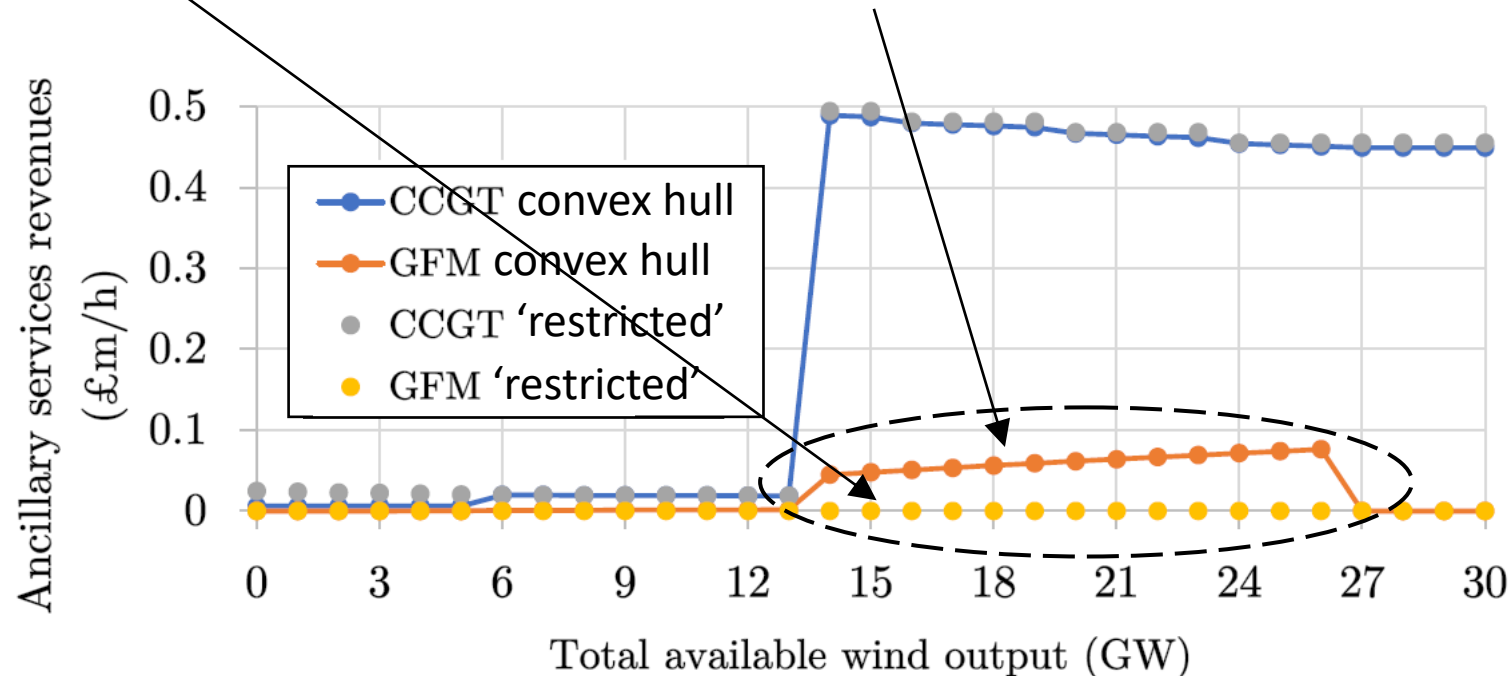
Price for synthetic inertia:

$$\frac{\mu - \lambda_1}{f_0} + 2\lambda_{\text{RoCoF}} - \lambda_{\text{q-s-s}} \cdot k_{\text{rec}}$$



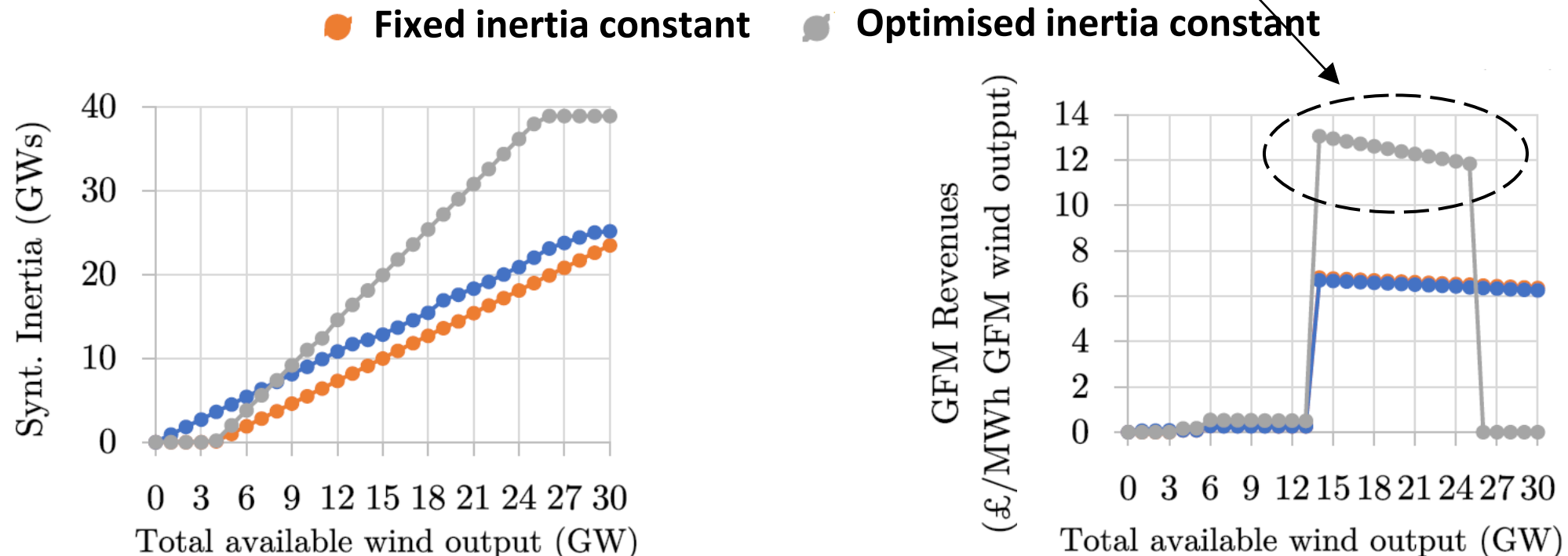
Challenge: **synchronous inertia** is linked to binary variables (i.e., **non-convexities**)

- ‘**Restricted pricing**’ (i.e. fixing the commitment decision of thermal units) **will not work** for remunerating RES providing frequency services
- **Convex hull pricing** is however **compatible with** remunerating **synthetic inertia**



The synthetic inertia constant is a **control parameter**:

- Synt inertia providers could **increase revenue by optimising**  $H_{\text{const}}$  hourly
- Requires a **communication network** (investment needed)



1. The theoretical framework when using **convex hull pricing needs development** (e.g., including AC OPF constraints)
2. Understand **implications** of this market **on other types of stability** (e.g., voltage and transient stability)
3. **Who should pay** for ancillary services?

# THANK YOU FOR YOUR ATTENTION!



Luis  
Badesa



Carlos  
Matamala



Yujing  
Zhou



Goran  
Strbac



LEADING INNOVATIONS FOR RESILIENT  
& CARBON-NEUTRAL POWER SYSTEMS  
25-29 JUNE, 2023, BELGRADE, SERBIA